

1 Derive continuity equation for regolith thickness

$$H(x, y, t) = H_0(x, y) + U(x, y, t) + V(x, y, t, H) \quad (1)$$

Where H_0 is the initial topography,

U is the vertical component of tectonic displacement,

and V is the geomorphic displacement.

Because U is the same for H and B at a given point (x, y) , it does not change the regolith thickness:

$$h(x, y) = (H(x, y) - U(x, y)) - (B(x, y) - U(x, y))$$

or

$$h(x, y) = H(x, y) - B(x, y)$$

Therefore, it is convenient to consider soil continuity in terms of soil thickness.

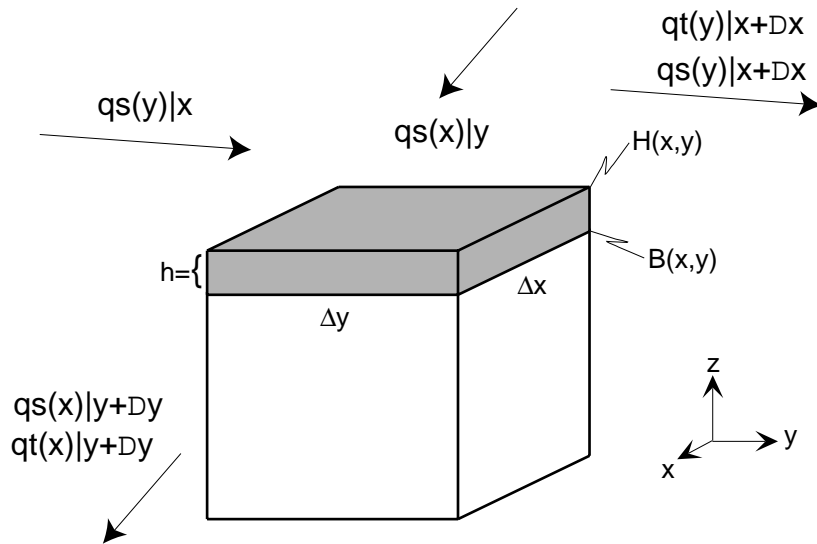


Figure 1: regolith continuity for a hillslope element

We use the derivation of conservation of transportable (regolith) for our control area (note that is a 2 dimensional problem):

$$\begin{aligned} & \left\{ \text{net rate of mass efflux from control area} \right\} + \\ & \left\{ \text{net rate of mass accumulation in control area} \right\} - \\ & \left\{ \text{rate of production of mass within control area} \right\} \\ & = 0 \end{aligned}$$

So let's take each term and evaluate it:

1. Net rate of mass efflux from control area. Consider the mass flux vector

$$\vec{n} = \rho \vec{v} = \rho_s \vec{q}_s \quad [ML^{-3} \cdot L^3 \cdot T^{-1}] \quad (2)$$

where ρ_s is sediment density $[ML^{-3}]$

\vec{q}_s is sediment volume flux $[L^3 T^{-1}]$

If we resolve the mass flux vector into its cartesian components, we have:

in the x direction: $n_x \Delta y|_{x+\Delta x} - n_x \Delta y|_x$

in the y direction: $n_y \Delta x|_{y+\Delta y} - n_y \Delta x|_y$

in the z direction: $n_z = 0$

2. Net rate of accumulation of mass in the control area:

$$\rho_s \frac{\partial h}{\partial t} \Delta x \Delta y \quad (3)$$

3. Net rate of production of mass in the control area:

$$-\rho_r \frac{\partial B}{\partial t} \Delta x \Delta y \quad \rho_r \text{ is the rock density} \quad (4)$$

Put it all together:

$$\begin{aligned} & \left\{ (n_x \Delta y|_{x+\Delta x} - n_x \Delta y|_x) + (n_y \Delta x|_{y+\Delta y} - n_y \Delta x|_y) \right\} + \\ & \rho_s \frac{\partial h}{\partial t} \Delta x \Delta y - \\ & -\rho_r \frac{\partial B}{\partial t} \Delta x \Delta y = 0 \end{aligned}$$

Divide through by $\Delta x \Delta y$ and simplify

$$\begin{aligned}
\left(\frac{\Delta n_x}{\Delta x} + \frac{\Delta n_y}{\Delta y}\right) + \rho_s \frac{\partial h}{\partial t} + \rho_r \frac{\partial B}{\partial t} &= 0 \\
\left(\frac{\partial}{\partial x} n_x + \frac{\partial}{\partial y} n_y\right) + \rho_s \frac{\partial h}{\partial t} + \rho_r \frac{\partial B}{\partial t} &= 0 \\
\nabla \vec{n} + \rho_s \frac{\partial h}{\partial t} + \rho_r \frac{\partial B}{\partial t} &= 0 \\
\rho_s \nabla \vec{q}_s + \rho_s \frac{\partial h}{\partial t} + \rho_r \frac{\partial B}{\partial t} &= 0
\end{aligned} \tag{5}$$

Thus (5) is the continuity equation for regolith thickness.

2 Evaluation of dimensions

If we look again at the first portion of (5),

$$\begin{aligned}
\left(\frac{\Delta n_x}{\Delta x} + \frac{\Delta n_y}{\Delta y}\right) + \rho_s \frac{\partial h}{\partial t} + \rho_r \frac{\partial B}{\partial t} &= 0 \\
\rho_s \left(\frac{\Delta q_{sx}}{\Delta x} + \frac{\Delta q_{sy}}{\Delta y}\right) + \rho_s \frac{\partial h}{\partial t} + \rho_r \frac{\partial B}{\partial t} &= 0
\end{aligned}$$

Focusing on the first term:

$$\rho_s \left(\frac{\Delta q_{sx}}{\Delta x} + \frac{\Delta q_{sy}}{\Delta y}\right) = \rho_s \nabla \vec{q}_s$$

Dimensionally:

$$[ML^{-3}] \left(\frac{[L^3 T^{-1}]}{[L]} + \frac{[L^3 T^{-1}]}{[L]} \right)$$

$$[ML^{-3}] ([L^2 T^{-1}] + [L^2 T^{-1}])$$

$$[ML^{-3}] [L^2 T^{-1}] = \rho_s \nabla \vec{q}_s$$

So, indeed

$$[L^2 T^{-1}] = \nabla \vec{q}_s$$